

Development of Anthropomorphic Robot Hand with Tactile Sensor : SKKU Hand II

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Abstract—In this paper, an anthropomorphic robot hand called SKKU Hand II is presented, which has a miniaturized fingertip tactile sensor. The thumb is designed as one part of the palm and provides the mobility of the palm. The fingertip tactile sensor, based on polyvinylidene fluoride(PVDF) and pressure variable resistor ink, is physically flexible enough to be deformed into any three-dimensional geometry. In order to detect incipient slip, a PVDF strip is arranged along the direction normal to the surface of the finger of the robot hand. Also, a thin flexible sensor to sense the static force as well as the contact location is fabricated into an arrayed type using pressure variable resistor ink. The driving circuits for the SKKU Hand II are embedded in the hand, and each driving circuit communicates with others using CAN protocol. In addition, a tactile sensing system is developed with miniaturized electronic hardwares such as charge amplifier, signal processing unit etc., and it is integrated into the robot hand. The SKKU Hand II is manufactured and feasibility of the hand and the fingertip tactile sensor is validated through preliminary experiments.

Index Terms—Anthropomorphic robot hand, Thumb, PVDF, Thin flexible force sensor, Tactile sensor.

I. INTRODUCTION

Recently, robots have begun to perform various tasks on replacing the human in the daily life such as cleaning, entertainments etc. In order to accomplish the effective performance of intricate and precise tasks, robot hand must have special capabilities, such as decision making in given condition, autonomy in unknown situation and stable manipulation of object. It must also possess tactile information to be able to carry out complicated manipulative tasks in a natural environment. Consequently, the tactile sensor is required to support natural interaction between the robot and the environment.

Many researches on the anthropomorphic multi-fingered robot hand have been reported up to now. The Utah/MIT hand developed by Jacobsen *et al.* is driven by actuators that are located in a place remote from the robot hand frame and connected by tendon cables [1]. Hirzinger *et al.* developed DLR-Hand II, which build the actuators into the hand. Each finger of robot hand is equipped with motors, 6-DOF fingertip force torque sensor and integrated electronics [3]. Kawasaki *et al.* presented anthropomorphic robot hand called the Gifu hand III, which has a thumb and four fingers. The thumb has 4 joints with 4-DOF and each of the fingers has 4 joints with 3-DOF. Moreover, the distributed tactile sensor which is

made of conductive ink is arranged about 859 sensing points on the palm and the fingers [4]. Shimojo *et al.* utilized the pressure conductive rubber as a pressure sensitive material. They attached the sensor onto a four finger robot hand and a demonstrated its grasping operations with a column, sphere, etc [5]. Although a number of researches have been done up to now, however, their motion of robot hands is unlike that of the human because the mechanism of robot hands is different from that of human in many aspects. A study on the grasping motion of the human hand noted that the metacarpal link of the thumb plays the key role in power grasping [6]. Despite these differences, However, many researches have been investigated about the robot hand of gripper type, which is difficult to perform dexterous grasping and manipulation of object like the human hand. Furthermore, most developed robot hands are larger than human hands. In addition, more researches are still necessary to put the tactile sensor into the practical use, because there remain many problems such as the limitations in the hardware as well as the algorithms for signal processing [7] [8].

In this paper, we propose an anthropomorphic robot hand called SKKU Hand II, which has a miniaturized tactile sensor applicable to the robot hand. Thumb is at an angle opposite to its other fingers, and the thumb and fingers are orthogonal, such that it can performs dexterous grasping and manipulation like the human hand. The hand is similar to the human hand in geometry and size because inessential degree-of-freedom is abbreviated during grasping. All parts of the SKKU Hand II were composed of independent modules from each finger to the electric board for control. Moreover, SKKU Hand II's fingertip tactile sensor is composed of two functional units: a PVDF-based slip sensor designed to detect slippage such as stick-slips between sensing elements and contact surfaces, and a thin flexible force sensor that can read the contact force of and geometrical information on the object using a pressure-variable resistor ink. The Actuators, driving circuits of SKKU Hand II and its entire sensing system are embedded in the hand, and each driving circuit communicates with others using CAN protocol.

This paper is organized as follows. In the section II and III, kinematic design and mechanical design of SKKU Hand II are presented. Also, system schematic of robot hand is described

in the section IV. The issues on the development of the PVDF texture sensor and thin flexible force sensor are discussed in the section V. In the section VI, experimental procedures for evaluation of the performance of the robot hand which has fingertip tactile sensors are mentioned. And finally the paper is concluded with summary in the section VII.

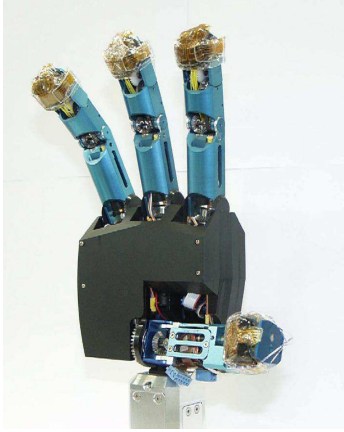


Fig. 1. SKKU Hand II with tactile sensor

II. KINEMATIC DESIGN OF SKKU HAND II

To develop the SKKU Hand II, the design process started with the simulation to get optimal ratios of link lengths of finger [9] [10]. We estimated an index of power grasping and fingertip grasping using kinetics model. Through the kinematic analysis and simulation, we decided that the ratio of length of link is 2-3-5 by Fibonacci sequence. Human hand is able to grasp objects by finger and thumb crossing each other to length way. The position of thumb and other finger is opposite to each other and thumb parallels other finger when gripper-type robot hand is grasping. However, in case of anthropomorphic robot hand, it grasps an object using the angle to direction of length of each finger for the power grasp and fingertip grasp. Especially, it has more powerful grasp by using the angle to direction of length of each finger in pinch grasp.

TABLE I
SPECIFICATION OF SKKU HAND II

	Joint	Gear	Torque [Nm]	Size [L × W][mm]	Weight [kg]
Finger	J1	275:1	0.115	115 × 22.5	0.116
	J2	258:1	0.106		
Thumb	J3	275:1	0.285	139 × 28	0.242
	J4	275:1	0.285		
	J5	258:1	0.106		
	J6	64:1	0.0297		
Total	-	-	-	-	0.9

III. THE MECHANICAL DESIGN OF SKKU HAND II

As shown in Fig. 1, the SKKU Hand II is designed to be anthropomorphic in terms of geometry, size, kinesis so that it performs power grasping and fingertip grasping as well as

manipulations like the human hand. Especially, all of the parts consist of modules for easy development, maintenance and repair.

A. Finger Module

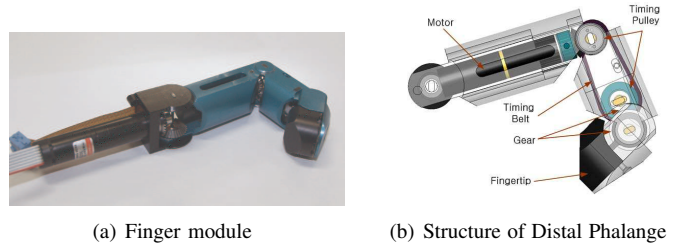


Fig. 2. Finger module

As shown in Fig. 2, the SKKU Hand II has three fingers, and it is about 1.1 times bigger than a human hand. Each finger module has total 3-DOF, including coupled joint of the last two joints, and degree of freedom of finger of robot hand is smaller than that of human finger and the difference is due to the reduction of unnecessary degree of freedom for the ability of grasp and maximization of efficiency with size of robot hand very close to that of human hand. The actuator of finger module has two electric motors. And every motor is installed possibly close to palm module in order to consider weight balance and kinesis. And the last two joints, Distal phalange and Medial phalange joint, are mechanically coupled like a human finger by the pulley and timing belt. Also it has some special space for being easy to install a variety sensors and the sensor processing circuit, in which for movement is more similar to human hand.

B. Thumb Module

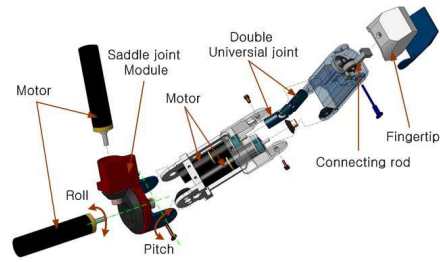


Fig. 3. Composition of thumb Module

The thumb module has four DOF, and it is about 1.1 times bigger than a human thumb. The thumb has played a very important part in the anthropomorphic robot hand as well as human hand. The thumb can fulfill a complex work by means of saddle joint that is closest to the wrist. In general, the saddle joint of human has 3-DOF, and it is possible to manipulate any motion in the three-dimensional space because the motion of pitch, roll and yaw is performed simultaneously. The motion

of pitch and roll is usually used to grasp the object, and the motion of yaw is used to circumvolve the object (precision grasp) motion like opening the cap of bottle. As depicted in Fig. 3 and 4, SKKU Hand II is realized with mechanism which imitates the role of saddle joint of human, but motion of yaw is neglected. The transmission of power is used with the bevel gear with 1:1 ratio, but distal phalange joint is composed of the Double Universal Joint so that the position of motor stays close to palm module and for the independence of actuators.

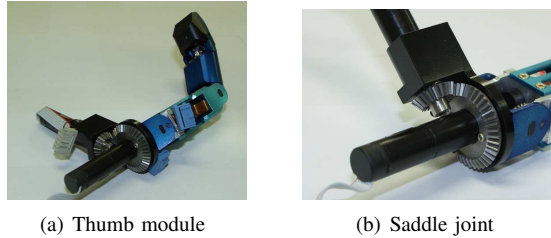


Fig. 4. Thumb Module

C. Fingertip Module



Fig. 5. The surface of fingertip depending on the grasping modalities

The shape of human fingertip is not just round but polyhedral. The surface of the fingertip can be discriminated into five parts depending on the grasping modalities such as pinch grasp, fingertip grasp and power grasp. As shown in Fig. 5, the fingertip grasp uses a bottom of fingernail, the pitch grasp that hold a small and long object strongly and safely uses a side of fingertip. In the power grasp which is for wrapping an arbitrary object, the object is restricted using bottom of finger, thumb, and palm, and then object is fixed by bottom of fingertip at last. Consequently, the fingertip of SKKU Hand II is designed as a unique shape which can realize composite task like fingertip of human.

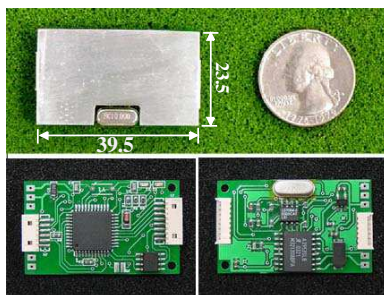


Fig. 6. Motor control board

D. Motor Control Board

Our anthropomorphic robot hand has the ten motor control boards. As shown in Fig. 6, each board size is 39.5 x 23.5 (mm) and every board is able to control just one corresponding motor. All of this board is composed independently from each other, but they are connected by CAN protocol. Also main microprocessor of Motor Control Board used PIC16F458 and the Motor control board includes the current sensor and counter chip to check the state of motor in real time. Each current sensor which can be utilized information of force feedback control with tactile sensor of fingertip is used to measure the torque of finger joint.

IV. CONTROL OF THE SKKU HAND II

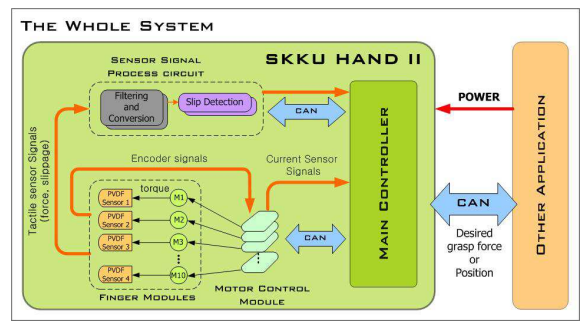


Fig. 7. System schematic of SKKU Hand II

The SKKU Hand II is able to control and communicate with motor control boards through CAN communication method. As shown in Fig. 7, motors are controlled by each independent motor control board respectively. If main control receives a message for control of finger from other application, this message is sent to each motor control board by the main controller. Then motor controllers control the motors of each finger using PID control. Force feedback control can be interpreted in the main controller using output signal of thin flexible force sensor, PVDF slip sensor which is embedded each fingertip and current sensor which is integrated motor controller, and then, feedback parameters is sent to motor control module.

V. TACTILE SENSOR OF SKKU HAND II

A. Slip sensor using PVDF

Since Kawai discovered strong piezoelectricity in PVDF in 1969, PVDF has been used in a lot of commercial products [11]. The voltage output of PVDF is 10 times higher than piezo-ceramics for the same force input [12]. The frame of PVDF strip is defined in terms of the length direction (direction 1), normal to the length direction in the plane of the film (direction 2) and normal to the plane of the PVDF strip (direction 3). When a PVDF strip is compressed by a probe on a rigid flat surface, assuming that both the flat surface and

the probe are friction-free, the film is free to expand along the 1-1 and 2-2 directions, the output charge can be expressed as

$$\frac{Q}{A} = d_{33}\sigma_3 = d_{33}\left(\frac{F}{A_3}\right) \quad (1)$$

$$Q = d_{33}F \quad (2)$$

where A_3 denotes the electroded area of the PVDF strip formed in the 3-3 plane, d_{33} represents the piezoelectric strain coefficient along the 3-3 direction, σ_{3n} is stress applied in the 3-3 direction. Therefore, the surface charge Q from the piezoelectric phenomena is proportional to the applied force F . Now, we explain the manufacturing and design of a miniaturized PVDF sensor with high sensitivity. Polyvinylidene fluoride pellets (Aldrich Chemical Co.) are pressed using a hot press machine. The thickness of fabricated films has a value between 50 and 70 μm . Then, the surface electrodes on both sides are fabricated using silk-screening technique with silver paste. By this method, a cost-effective and simple fabrication process is secured. In order to exhibit high piezoelectricity in the fabricated films, the fabricated PVDF film is polarized by applying the strong electric field using the high voltage supply. As shown in Fig. 8, the PVDF sensor consists of single PVDF strip with the thickness of 100 μm , 0.8mm width and 10mm length, where the sensing element has the size of 0.4mm \times 4mm.

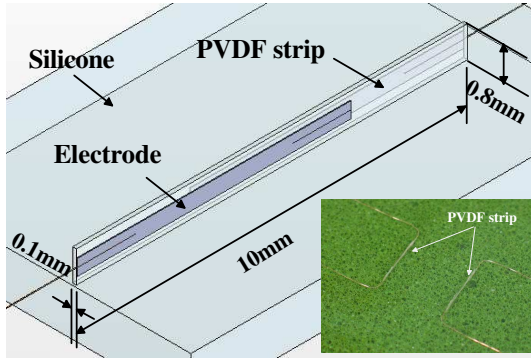


Fig. 8. Schematic of PVDF sensor and photograph

B. Thin flexible force sensor

PVDF is adequate for sensing dynamic force, not the static one. In this research, pressure variable resistor ink (Creative Materials Inc.) is used to develop a force sensor. Pressure variable resistor ink is an electrically conductive ink, where its resistance decreases as the pressure goes up. The force sensor is fabricated by sandwiching the ink between two polyester films with the pattern of electrodes. When the fixed input voltage is applied to the sensor, it can read the change of the output value amplified by the voltage gain. Thus, the output is written by

$$V_{out} = -V_{cc}\frac{R_F}{R_s} = -V_{cc}R_F S_s \quad (3)$$

where R_s is resistance of force sensor, S_s denotes the conductance, that is, the reciprocal of resistance. Also, R_F is the op-amp's feedback resistance.

To develop a force sensor with high resolution, the electrode pattern of the grid type is adopted in this research. The two polyester films are aligned as a grid while the pressure variable resistor ink layers face each other. Thus, each cross section of the grid forms single sensing element of the force sensor. As shown in Figs. 9 and, the size of each sensing element is 0.5mm \times 0.5mm and the total number of sensing elements goes up to 24. In the current approach, it is possible to read 24 sensing elements only with 8 input voltage lines and 4 output signal lines although the timing circuit is required.

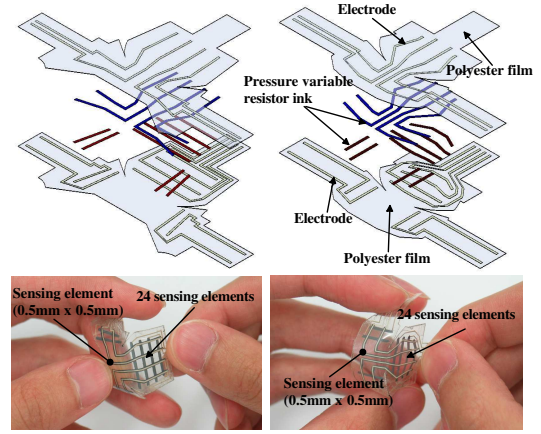


Fig. 9. Fingertip force sensor

C. Integrated tactile sensor

The fingertip tactile sensor consists of two different sensing elements, that is a thin flexible force sensor for detecting the contact force and location and the PVDF sensor for incipient slip. The structure of the fingertip tactile sensor is shown in Fig. 10. Thin flexible force sensor which possesses 24 sensing elements is attached under the fingertip to detect static contact force. Also, the PVDF sensor which has two PVDF strips is located on the thin flexible force sensor to detect dynamic response such as slippage using the mechanical deformation of the silicone.

D. Hardware for signal processing

In this section, we introduce the miniaturized electronic hardware to be utilized for signal processing. Two signal amplifiers have been developed in this research. One of them is for the PVDF sensor and the other for the force sensor. The amplifier for PVDF sensor is basically used to convert the minute charge output from the PVDF strip into the voltage signal. The circuit for the PVDF sensor amplifier with the size

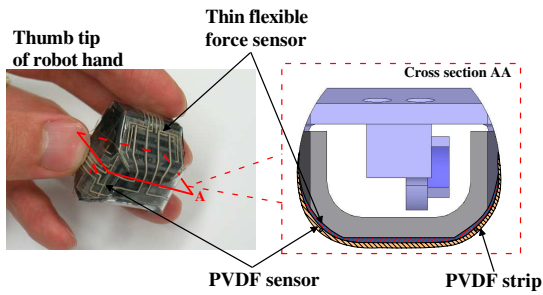


Fig. 10. Structure of fingertip tactile sensor

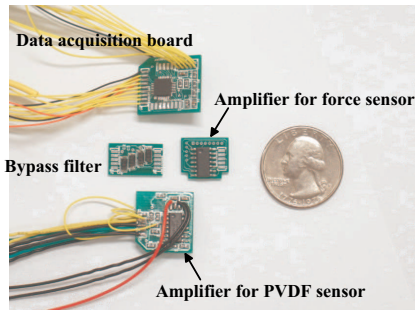


Fig. 11. Photograph of tactile sensing system

of $18\text{mm} \times 14\text{mm}$, consists of charge amplifier, non-inverting amplifier and 60 Hz notch filter. Different from the PVDF sensor amplifier, the force sensor amplifier just amplifies the output voltage of the sensor using an Op-amp. The circuit for the signal processing is designed on single board for data acquisition, control, communication. Data acquisition and communication are performed by using microcontroller (C8051F311). The signal processing board is able to transmit data to the PC via RS232 or SMBus. The microprocessor in the signal processing unit is able to receive amplified output signals from each sensing element by periodical scanning. The amplified signals are transformed into digital data with the A/D converter which is included in the microcontroller. Therefore, the developed configuration of the force sensor and slip sensor can effectively control all the sensing elements by using the minimum number of input and output signal lines.

VI. EXPERIMENTS

In the first experiments, the sensor was touched and rubbed after installing on the fingertip. As shown in Fig. 12, it is noted that there exists the sharp change of signals, which implies that stick-slip occurred between the sensor and the contact surface. Also, the weight of 100g was rolled on the PVDF sensor. As shown in Fig. 13, the effect of stick-slip was not found and the smoother patterns of the signal compared to Fig. 12, was observed. When the weight of 100g rolled on the sensing element the output indicated about 1.2V constantly. Consequently, it is concluded that the characteristic of response can be discriminated depending on the surface characteristics of the object and the contact method, although calibrations are still needed.

In the second, the force sensor was tested. Static loads with the weight of 100g and 200g were applied, and the responses were obtained. As shown in Fig. 14, the output voltages of 2V and 4.25V were obtained for each weight. It is noted that the output has linear relation with the weight. Before the integrated tactile sensor was attached to the robot hand, the SKKU Hand II was tested by grasping a bottle. As shown in Fig. 15, it is possible to confirm that the developed robot hand can grasp the bottle stably. Finally, the overall sensing system was tested by attaching it to the robot hand. We confirmed the contact information through the user interface on the PC as shown in Fig. 16(a). It shows the contact information when we pressed the sensor in the fingertip. According to display of the user interface, the output distribution changes and the PVDF sensor responded to the stimuli sensitivity. In addition, Fig. 16(a) shows the contact information when robot hand grasped the bottle using the power grasping. According to the contact condition between sensing elements and contact surfaces of bottle, each fingertip sensor shows corresponding response. Therefore, it is possible to confirm that the each fingertip tactile sensor can detect the static force, location of contact and slippage.

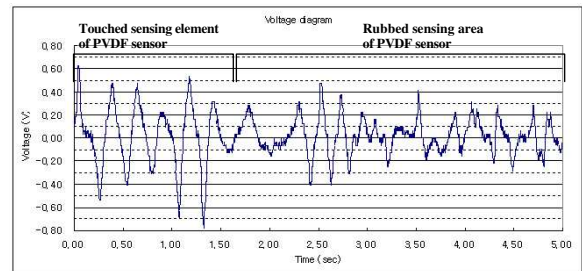


Fig. 12. Signal output from touching and rubbing.

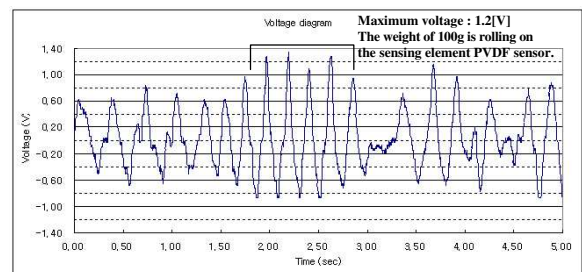


Fig. 13. Signal output from rolling of 100g weight.

VII. CONCLUSION

In this research, an anthropomorphic robot hand called SKKU Hand II was developed. Different from the previous gripper-type robot hands, the thumb of SKKU Hand II is designed as one part of the palm and provides the mobility of the palm. The robot hand is actuated by built-in DC motors,

and fingertip tactile sensors are attached to its fingertips. A tactile sensor which can detect contact normal forces as well as slip is made of two organic materials, such as polyvinylidene fluoride (PVDF) that is known as piezoelectric polymer, and pressure variable resistor ink. The motor control boards and sensing systems were miniaturized as small as to be integrated into the robot hand. The SKKU Hand II which integrated fingertip tactile sensors is validated through preliminary experiments. In the next research, we will control the robot hand for dexterous grasping and manipulation using the force feedback from the fingertip tactile sensors and evaluation will be performed.

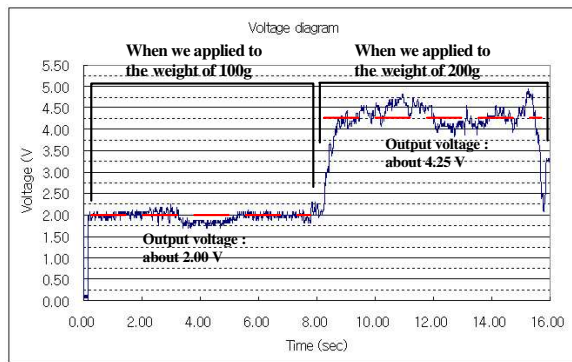


Fig. 14. When we applied to the weight of 100g and 200g.

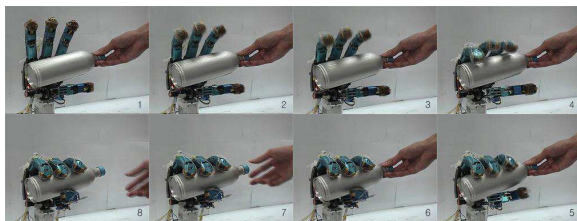


Fig. 15. Movement of SKKU Hand II.

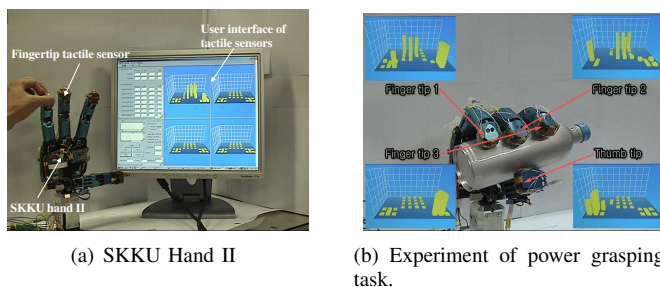


Fig. 16. Experiments of SKKU Hand II with fingertip tactile sensors

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REFERENCES

- [1] S. C. Jacobsen *et al.*, "The Utah/MIT dexterous hand: Work in progress", *Int. J. Robot. Res.*, vol. 3, no. 4, pp. 21-50, 1984.
- [2] S. C. Jacobsen, I. D. McCammon, K. B. Begg, and R. P. Phillips, "Design of Tactile Sensing Systems for Dexterous Manipulator", *IEEE Control Syst. Mag.*, vol. 8, issue. 1, pp. 3-13, 1988.
- [3] J. Butterfass, M. Grebenstein, H. Liu, G. Hirzinger, "DLR-Hand II: Next Generation of a Dexterous Robot Hand", *Proc. of IEEE Int. Conf. on Robotics and Automation*, vol. 1, pp. 109-114, 2001.
- [4] H. Kawasaki, T. Komatsu, K. Uchiyama, "Anthropomorphic Robot Hand: Gifu Hand III", *Int. conf. on Control, Automation, and Systems*, pp. 1288-1293, 2002.
- [5] M. Shimojo, A. Namiki, M. Ishikawa, R. Makino, and K. Mabuchi, "A Tactile Sensor Sheet using Pressure Conductive Rubber with Electrical-Wires Stitched Method", *IEEE Sensors Journal*, vol. 4, no. 5, pp. 589-596, 2004.
- [6] B. Calais-Germain, *Anatomy of movement*, Eastland Press, 1993.
- [7] H. R. Nicholls and M. H. Lee, "A survey of robot tactile sensing technology", *Int. J. Robot. Res.*, vol. 8, no. 3, pp. 3-30, 1989.
- [8] M. H. Lee and H. R. Nicholls, "Tactile sensing for mechatronics-A state of the art survey", *Mechatronics*, vol. 9, pp. 1-31, 1999.
- [9] K. J. Kyriakopoulos, J. V. Raper, A. Zink, H. E. Stephanou, "Kinematic Analysis and Position/Force Control of the Anthropomorphic Hand", *IEEE/ASME Transactions on Systems, Man And Cybernetics*, Vol. 27, pp. 95-104, 1997.
- [10] D. Wilkinson, M. V. Weghe, Y. Matsuoka, "An Extensor Mechanism for an Anatomical Robotics Hand", *Proc. of IEEE Int. Conf. on Robotics and Automation*, pp. 238-243, 2003.
- [11] H. Kawai, "The Piezoelectricity of Poly(vinylidene fluoride)", *Jpn. J. Appl. Phys.*, vol. 8, pp. 975-976, 1969.
- [12] J. Fraden, *Handbook of Modern Sensors: Physics, Designs, and Applications*, American Institute of Physics Press, 1997.
- [13] B. J. Choi, S. C. Kang, and H. R. Choi, "Development of Tactile Sensor for Detecting Contact Force and Slip", *Proc. of IEEE/RSJ Int. conf. on Intelligent Robots and Systems*, pp. 1977-1982, 2005.
- [14] J. Butterfass, M. Grebenstein, G. Hirzinger, H. Liu, "DLR-Hand II : Next Generation of a Dexterous Robot hand", *Proc. of IEEE/RSJ Int. Conf. on Robotics and Automation*, pp. 109-114, 2001.
- [15] X. H. Gao, M. H. Jin, L. Jiang, Z. W. Xie, P. He, L. Yang, M. Grebenstein, G. Hirzinger, "The HIT/DLR Dexterous Hand: Work in Progress", *Proc. of IEEE Int. Conf. on Robotics and Automation*, pp. 3164-3168, 2003.
- [16] I. Yamano, K. Takemura, T. Maeno, "Development of a Robot Finger for Five-fingered Hand using Ultrasonic Motors", *Proc. of IEEE/RSJ Int. Conf. on Robotics and Automation*, vol. 23, no. 4, pp. 2648-2563, 2003.
- [17] P. Dario and G. Buttazzo, "An Anthropomorphic Robot Finger for Investing Artificial Tactile Perception", *Int. J. Robotics. Res.*, vol. 6, no. 3, pp. 25-48, 1987.
- [18] R. D. Howe and M. R. Cutkosky, "Dynamic Tactile Sensing: Perception of Fine Surface Features with Stress Rate Sensing", *IEEE Transaction on Robotics and Automation*, vol. 9, no. 2, pp. 140-151, 1993.
- [19] I. Fusijimoto, Y. Yamada, T. Maeno, "Development of Artificial Finger Skin to Detect Incipient Slip for Realization of Static Friction Sensation", *Proc. of IEEE Int. Conf. on Multisensor Fusion and Integration for Intelligent Systems, MFI2003*, pp. 15-20, 1999.
- [20] Y. Tada, K. Hosoda, Y. Yamasaki, M. Asada, "Sensing the Texture of Surfaces by Anthropomorphic Soft Fingertips with Multi-modal Sensors", *Proc. IEEE/RSJ Int. Conf. on Intelligent Robots and Systems*, vol. 1, pp. 31-35, 2003.
- [21] R. A. Russell, *Robotic Tactile Sensing*, Prentice Hall, Inc, 1990.
- [22] C. M. A. Ashruf, "Thin flexible pressure sensor", *Sensors Review*, vol. 22, no. 4, pp. 322-327, 2002.
- [23] K. H. Yu, T. G. Kwon, M. J. Yoon, S. C. Lee, "Development of a Tactile Sensor Array with Flexible Structure using Piezoelectric Film", *KSME International Journal*, vol. 16, no. 10, pp. 1222-1228, 2002.